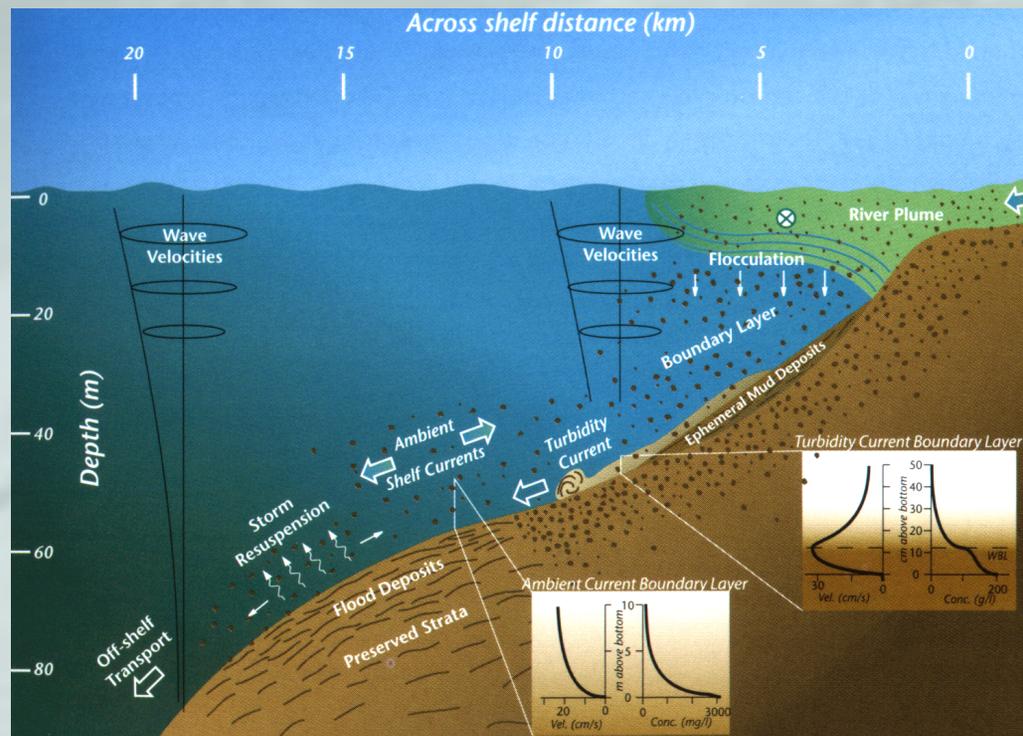


# Earth-surface Dynamics Modeling & Model Coupling

## *A short course*

*James PM Syvitski & Eric WH Hutton, CSDMS, CU-Boulder*

With special thanks to Pat Wiberg, Carl Friedrichs, Courtney Harris, Chris Reed, Rocky Geyer, Alan Niedoroda, Rich Signell, Chris Sherwood



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## Module 5: Shelf Sediment Transport

ref: Syvitski, J.P.M. et al., 2007. Prediction of margin stratigraphy. In: C.A. Nittrouer, et al. (Eds.) Continental-Margin Sedimentation: From Sediment Transport to Sequence Stratigraphy. IAS Spec. Publ. No. 37: 459-530.

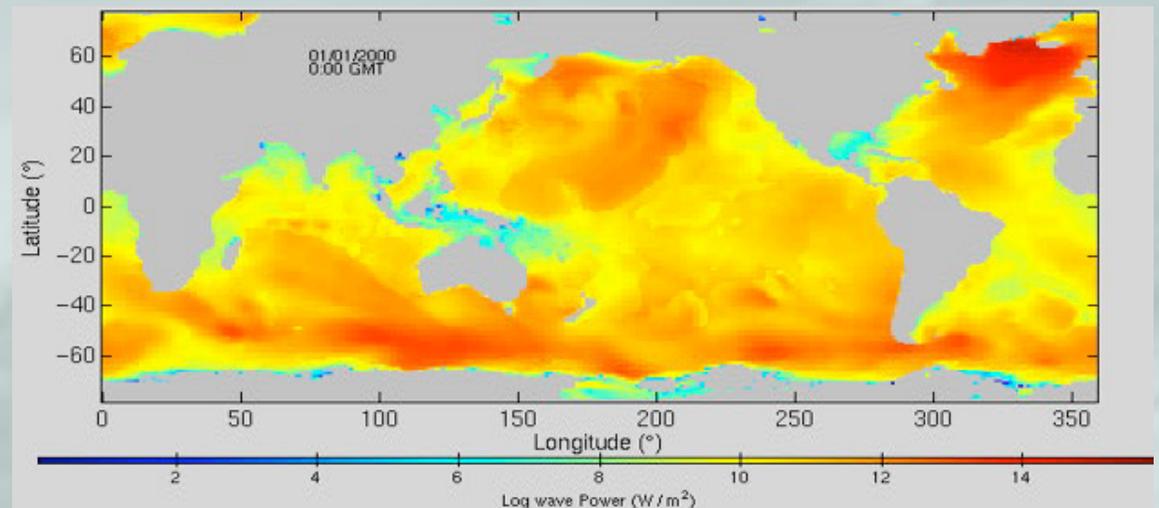
Shelf diffusivity (3)

Gravity-driven slope equilibrium (4)

Event-based models (7)

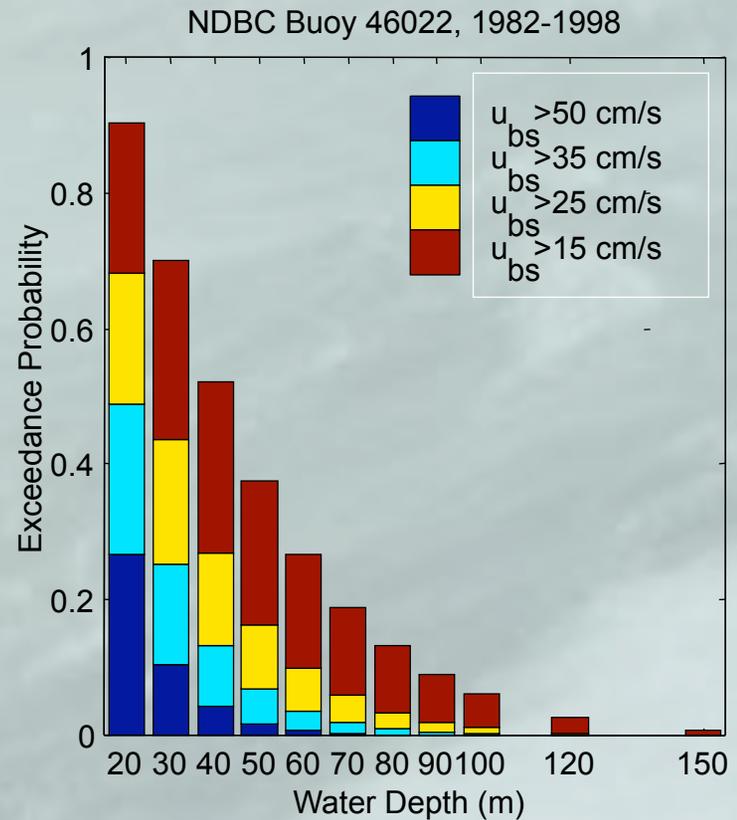
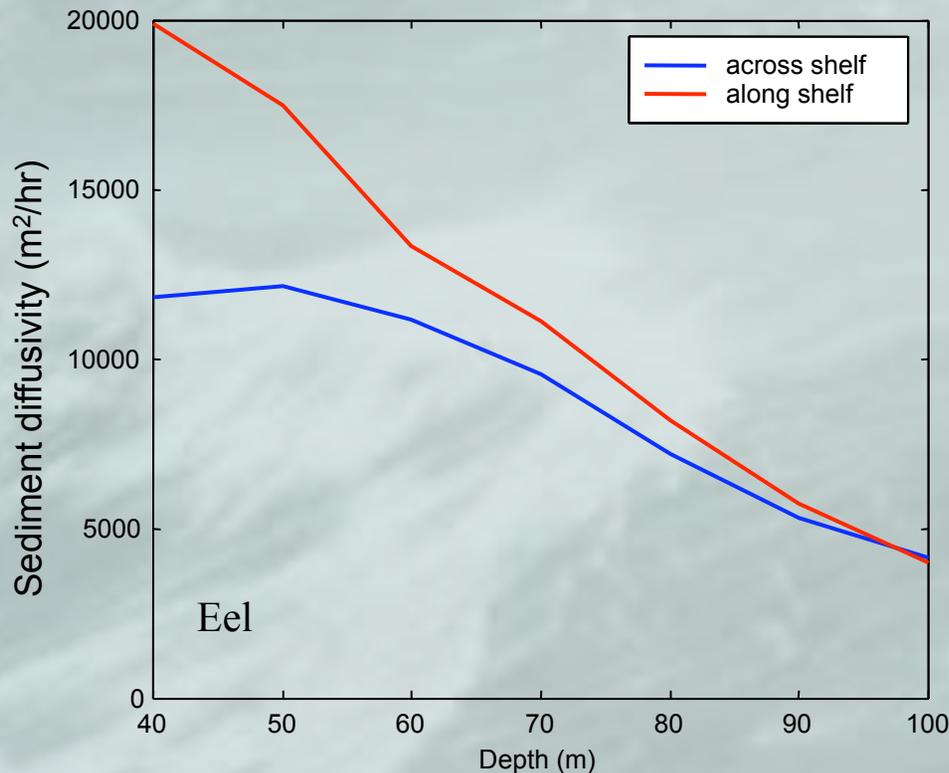
Coastal Ocean Models (4)

Summary (1)



# Shelf diffusivity

Local transport occurs if the probability of wave resuspension is exceeded at a particle's water depth.



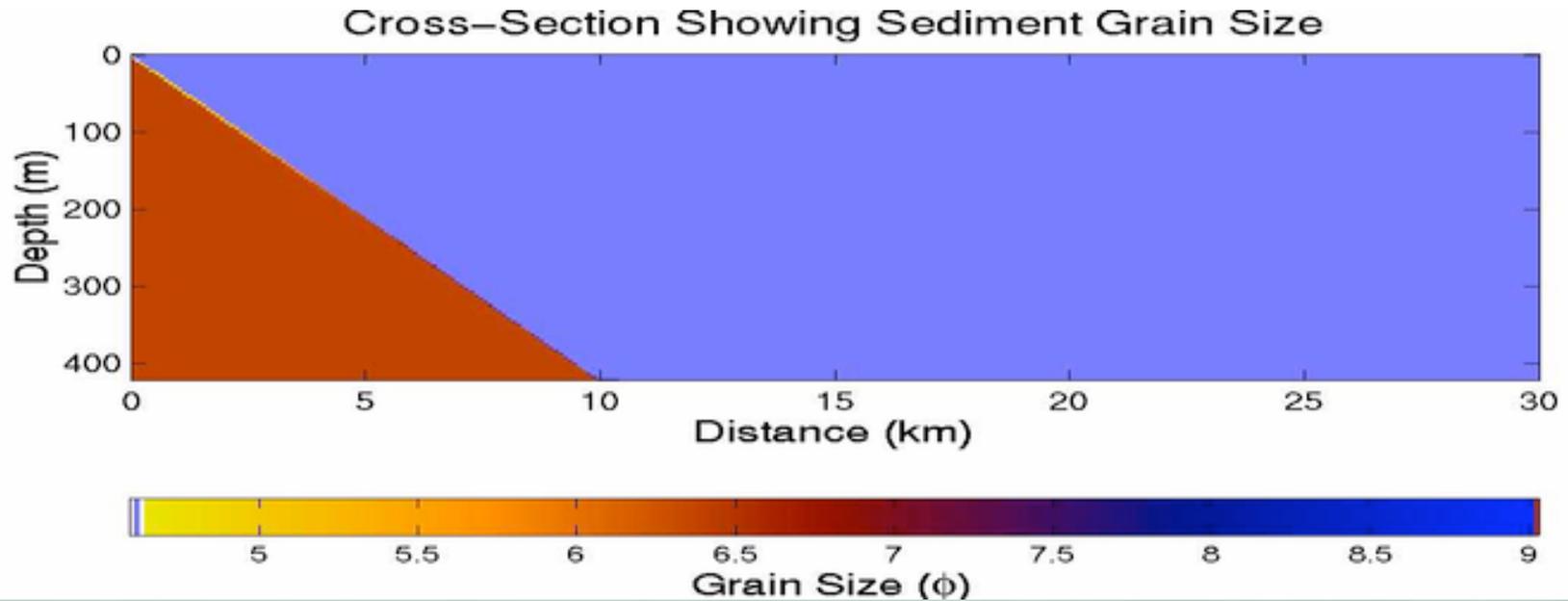
# Shelf diffusivity

*Resuspension and Advection by Bottom Boundary Energy*

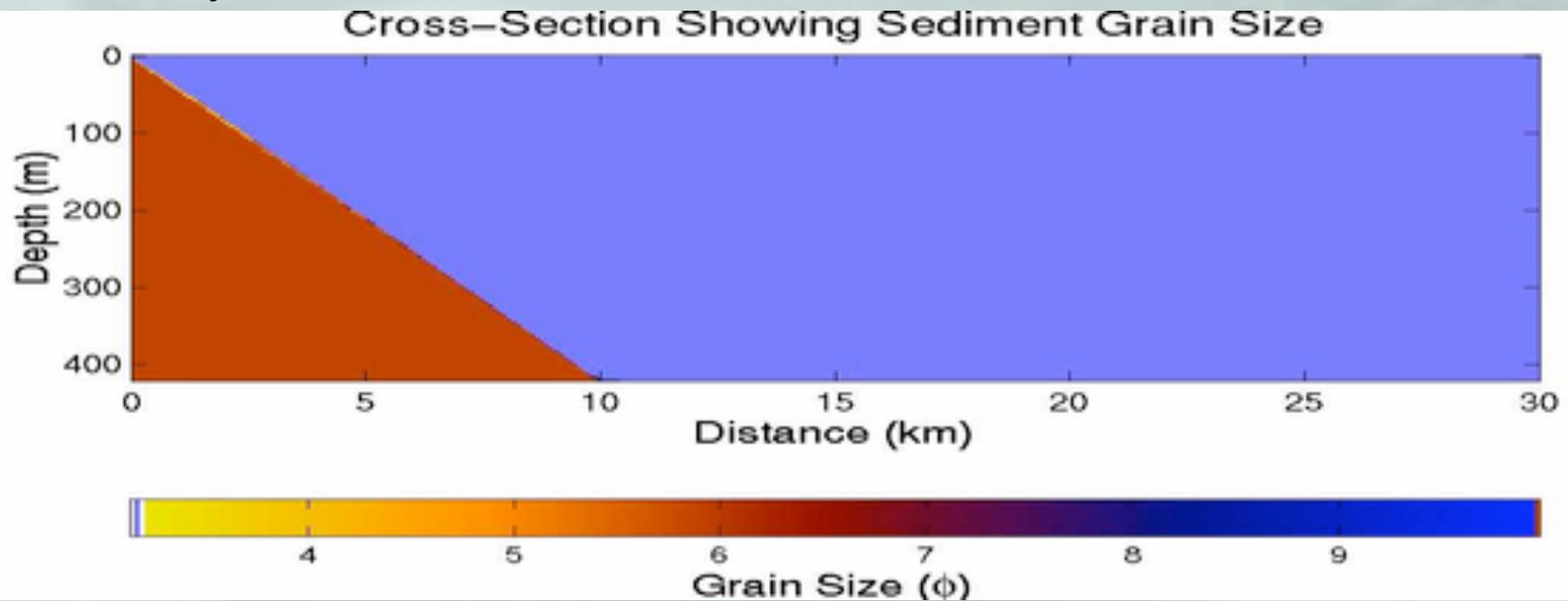
$$\frac{\partial h}{\partial t} = \frac{\partial}{\partial x} \left( k(t, x) \frac{\partial h}{\partial x} \right) \quad \frac{\partial h_i}{\partial t} = \tilde{k}_i \frac{\partial h}{\partial t}$$

- $k(t, z)$  varies over time  $t$  (pdf of storms), and water depth  $z$ . Following Airy wave theory,  $k$  falls off exponentially with water depth.
- $k_i$  is an index between 0 and 1 that reflects the ability of grain size  $i$  to be resuspended and advected.
- $k(t, z) \geq k_i$  for sediment transport



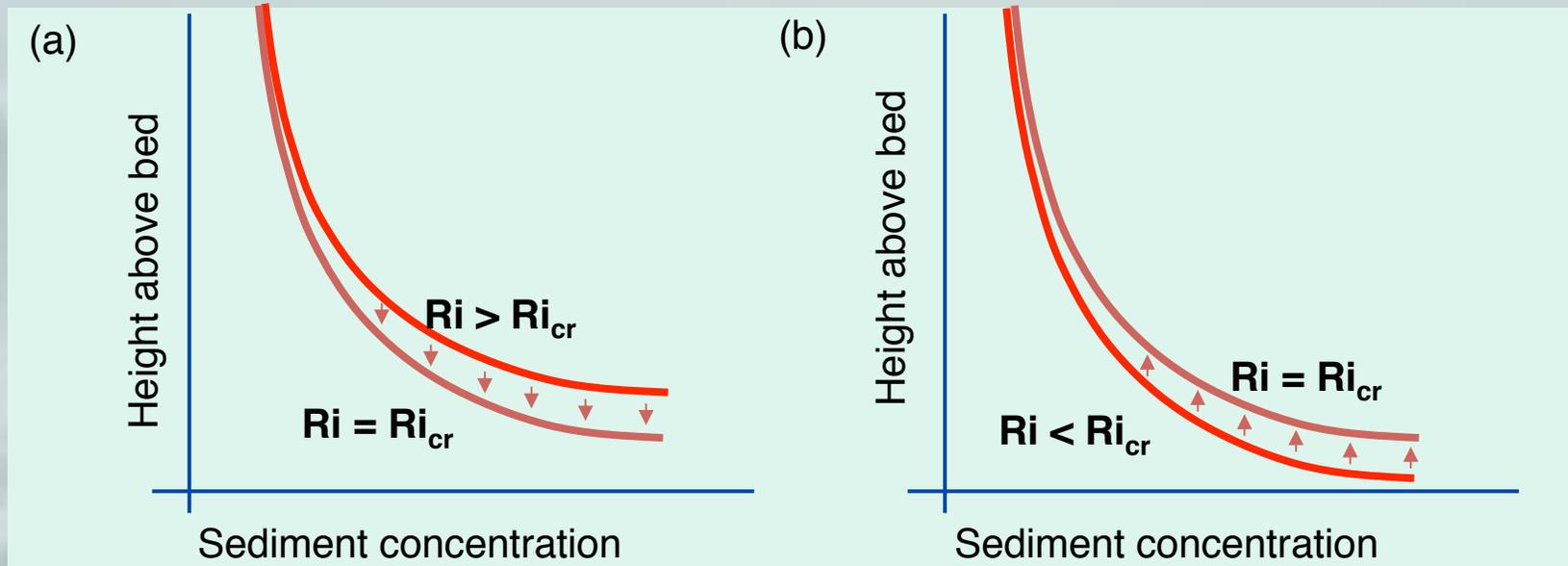


Plumes Only



# Gravity-driven slope equilibrium

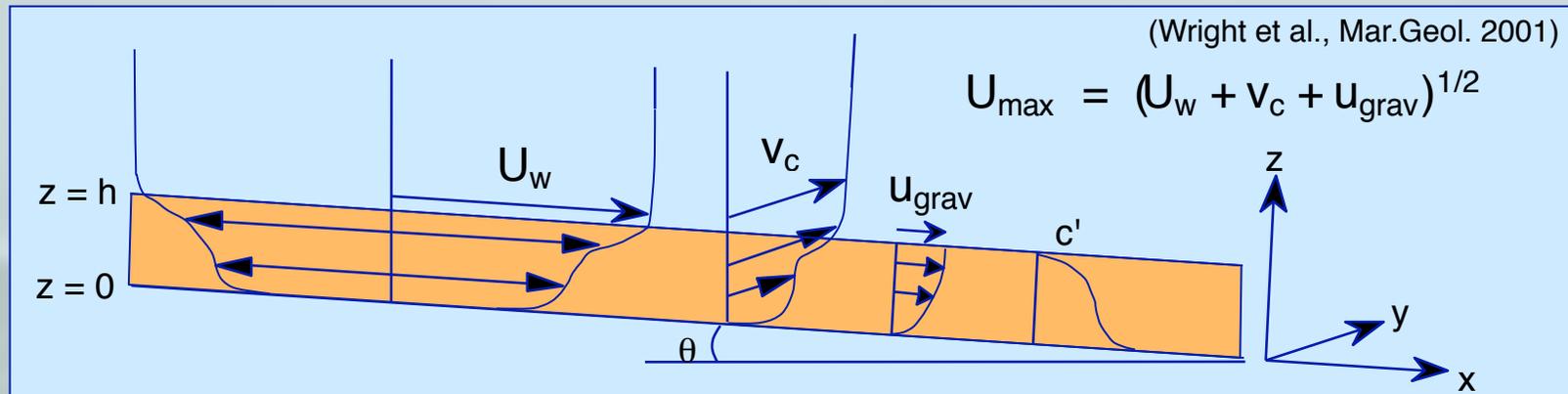
Gradient Richardson Number ( $Ri$ ) =  $\frac{\text{density stratification}}{\text{velocity shear}}$  Shear instabilities occur for  $Ri < Ri_{cr}$   
 “ “ suppressed for  $Ri > Ri_{cr}$



- (a) If excess sediment enters BBL &  $Ri$  increases beyond  $Ri_{cr}$ , then turbulence is dampened, sediment is deposited, stratification is reduced and  $Ri$  returns to  $Ri_{cr}$
- (b) If excess sediment settles out of boundary layer, or bottom stress increases &  $Ri$  decreases beyond  $Ri_{cr}$ , then turbulence intensifies. Sediment re-enters base of boundary layer. Stratification is increased in boundary layer and  $Ri$  returns to  $Ri_{cr}$ .



# Gravity-driven slope equilibrium



## (i) Momentum balance:

Down-slope pressure gradient = Bottom friction

$$\alpha B = c_d \langle |u| u \rangle = c_d U_{\max} U_{\text{grav}}$$

x-shelf bed slope  $\rightarrow$   $\alpha B$  = depth-integrated buoyancy anomaly  
 $c_d$  = bottom drag coefficient  
 $\langle |u| u \rangle$  = wave-averaged, x-shelf component of quadratic velocity  
 $U_{\max}$  = total velocity =  $(U_w^2 + v_c^2 + U_{\text{grav}}^2)^{1/2}$   
 $U_{\text{grav}}$  = x-shelf gravity flow velocity

## (ii) Maximum turbulent sediment load:

(c.f. Trowbridge & Kineke, JGR 1994)

$$\text{Richardson Number} = \frac{\text{Buoyancy}}{\text{Shear}} = \text{Critical value} \quad \text{Ri} = \frac{B}{(U_{\max})^2} = \text{Ri}_{\sigma} = 1/4$$

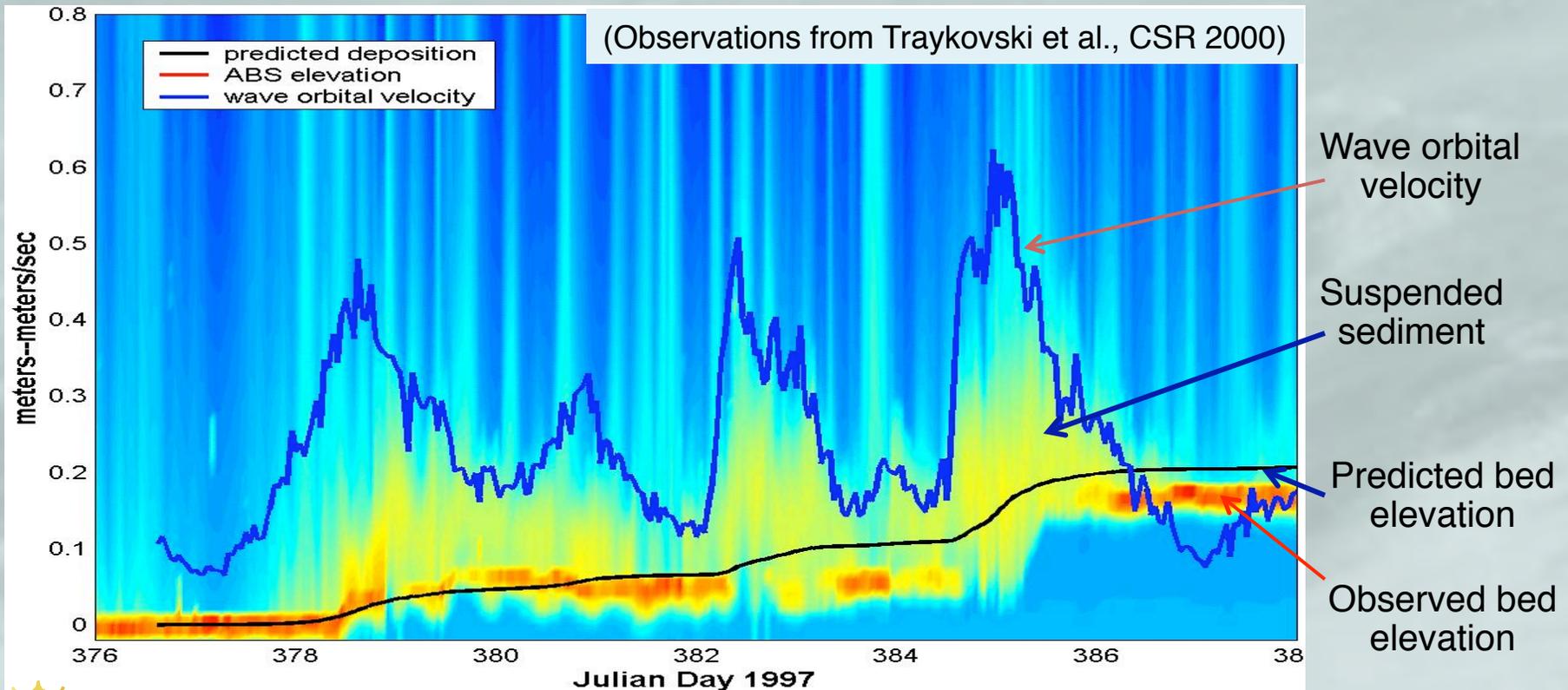


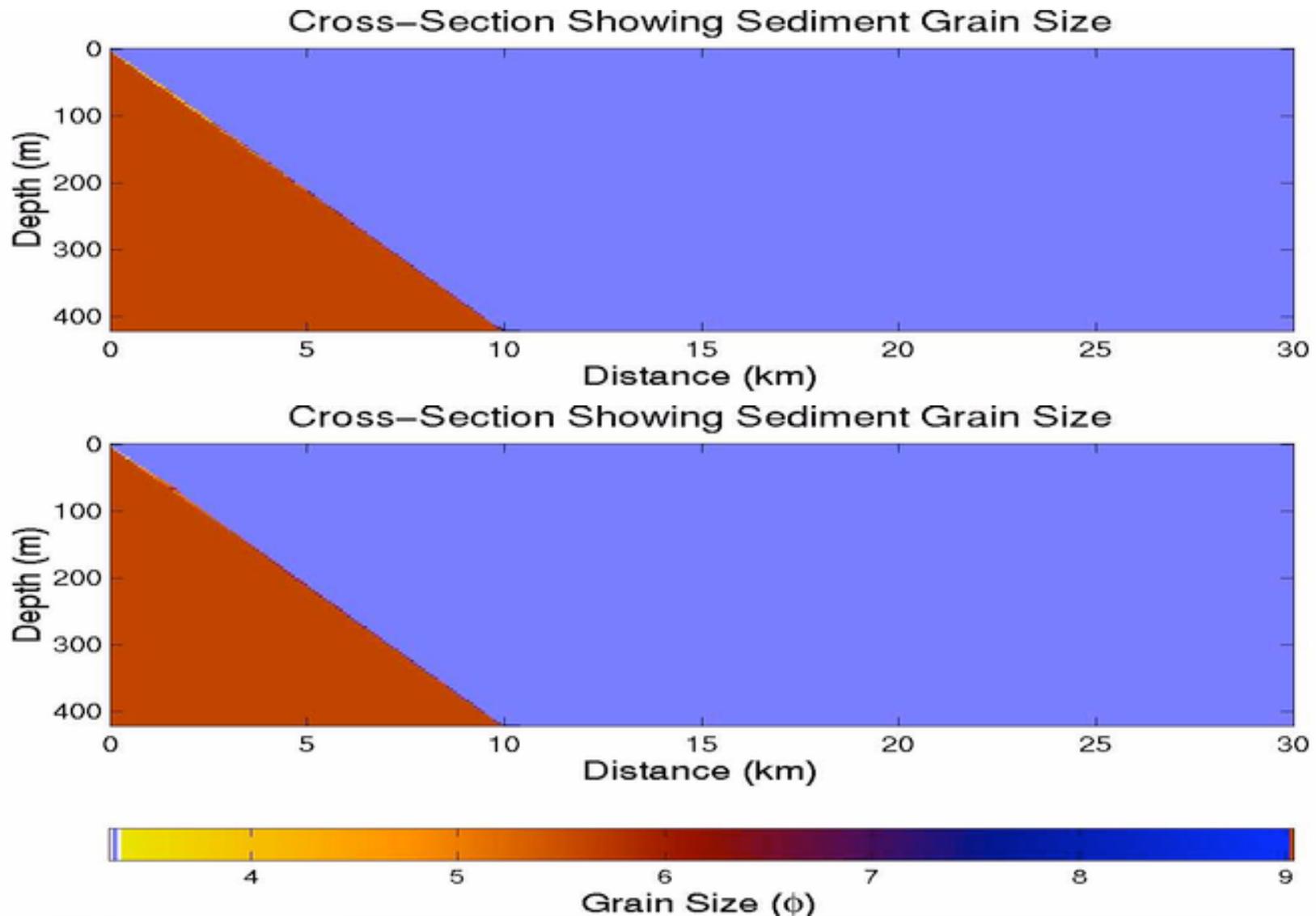
# COMPARISON OF MODEL PREDICTIONS TO OBSERVED DEPOSITION

Application to 1996-97 Eel River Flood at 60-meter Site

$$\text{Deposition Rate} = - \frac{Ri_{cr}^2}{(1-P) c_d g s} \frac{d}{dx} (\propto U_{max}^3)$$

|                     |  |                               |   |                                       |
|---------------------|--|-------------------------------|---|---------------------------------------|
| Porosity<br>P = 0.9 | $(\rho_{sed}/\rho_{water} - 1)$<br>s = 1.6 | Bed slope<br>$\alpha = 0.004$ | Richardson #<br>Ri <sub>cr</sub> = 0.25 | Drag coeff.<br>c <sub>d</sub> = 0.003 |
|---------------------|--|-------------------------------|---|---------------------------------------|



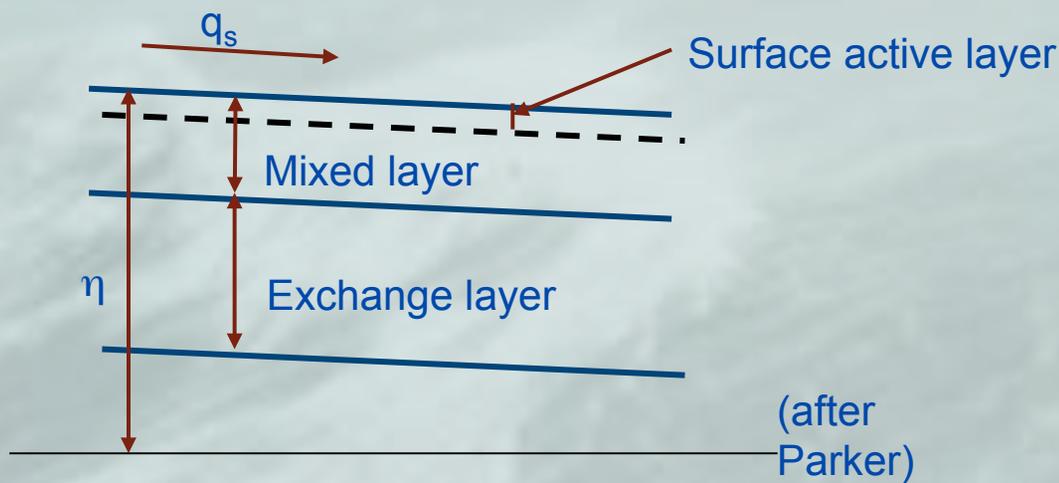


Top: Plumes & Wave Diffusion; Bottom: Plumes, Waves & Fluid Muds



# Event-based transport model

Calculate suspended sediment flux (by grain size) using a 1-D shelf sediment transport model at a cross-shelf grid of nodes of specified depth and sediment characteristics. For each event (set of wave & current conditions), the net flux is calculated at each node. The divergence of the flux gives the change in bed elevation.



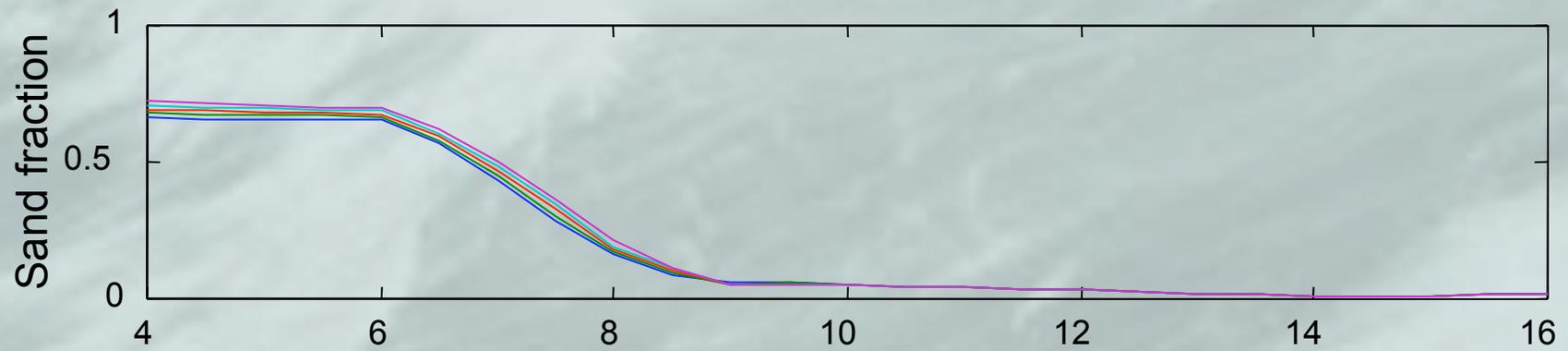
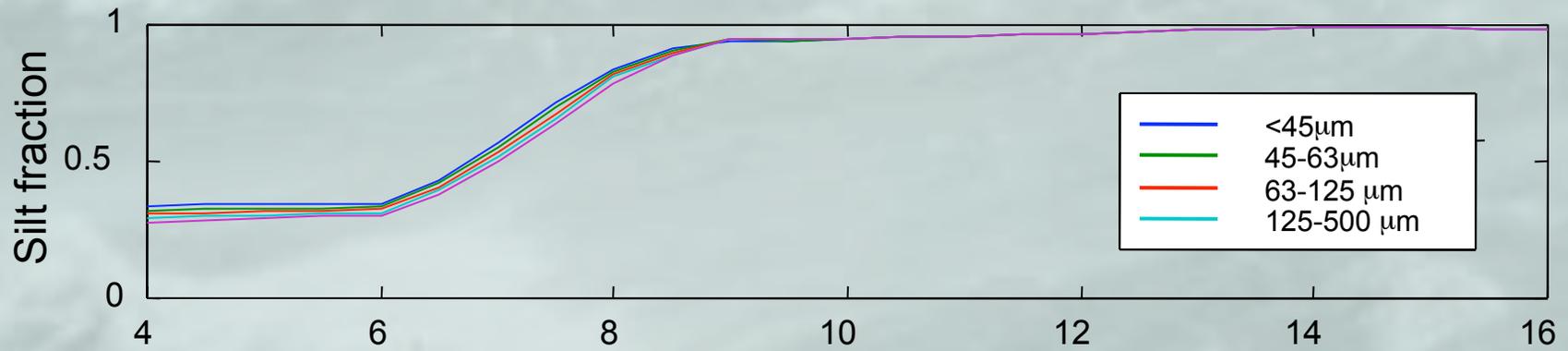
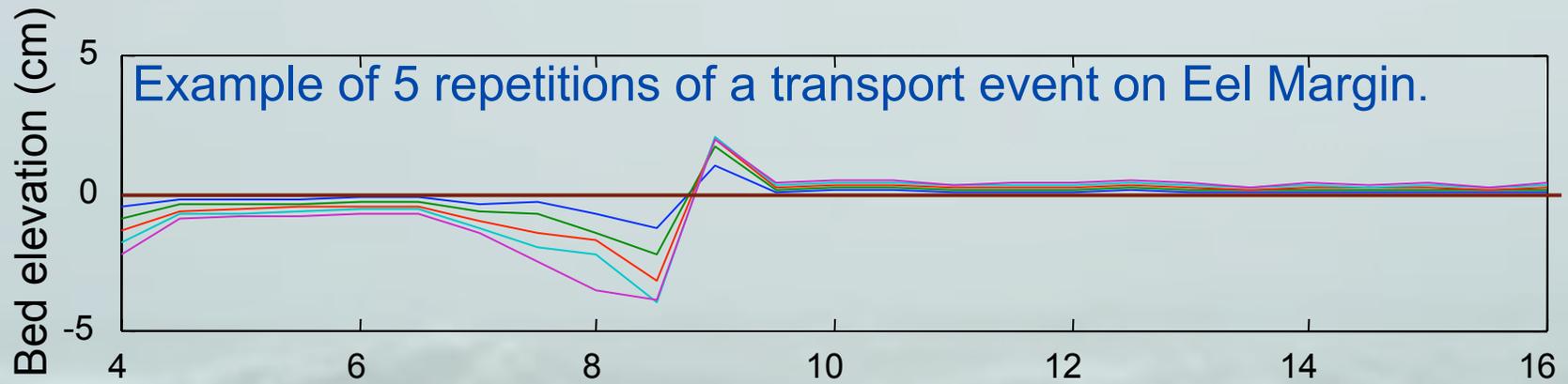
$$q_{xi} = -D_{cx} \frac{\partial c_i}{\partial x} \quad q_{yi} = -D_{cy} \frac{\partial c_i}{\partial y}$$

$$\frac{\partial \eta_i}{\partial t} = -\frac{1}{c_b} \left( \frac{\partial}{\partial x} D_{cx} \frac{\partial c_i}{\partial x} + \frac{\partial}{\partial y} D_{cy} \frac{\partial c_i}{\partial y} \right)$$

$$\frac{\partial \eta}{\partial t} = \sum_{i=1}^N \frac{\partial \eta_i}{\partial t}$$

$$\frac{\partial F}{\partial t} = -\frac{1}{c_b L_a} \left( \frac{\partial q_i}{\partial x} \right) - \left( F_{ei} \frac{\partial \eta}{\partial t} + \sigma \right)$$



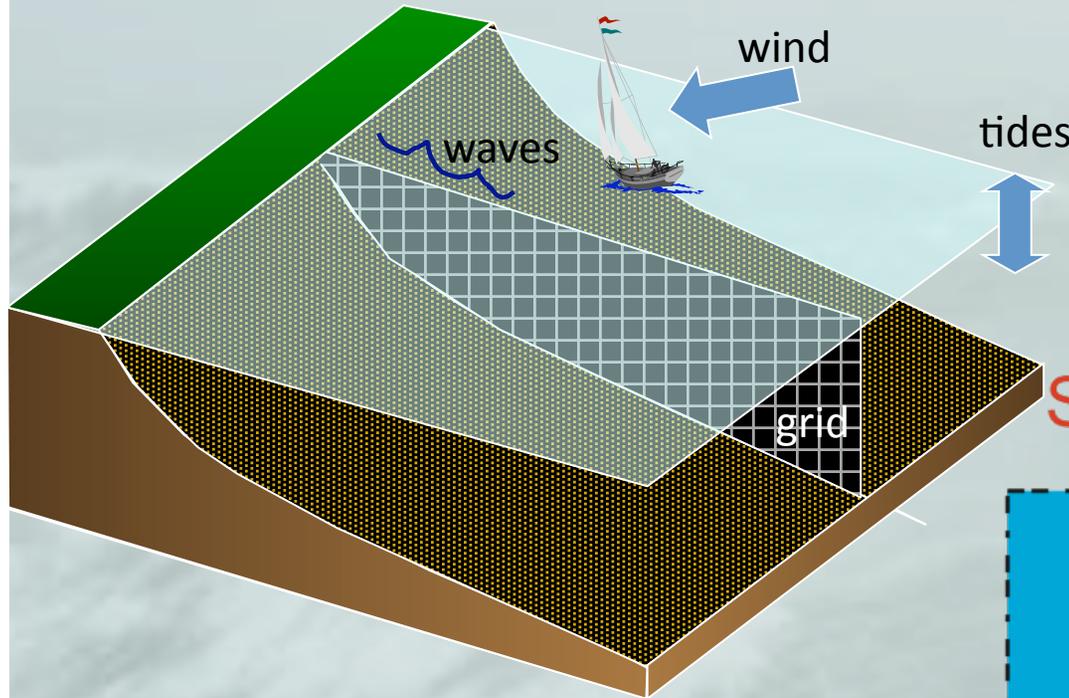


Cross-shelf distance (km)

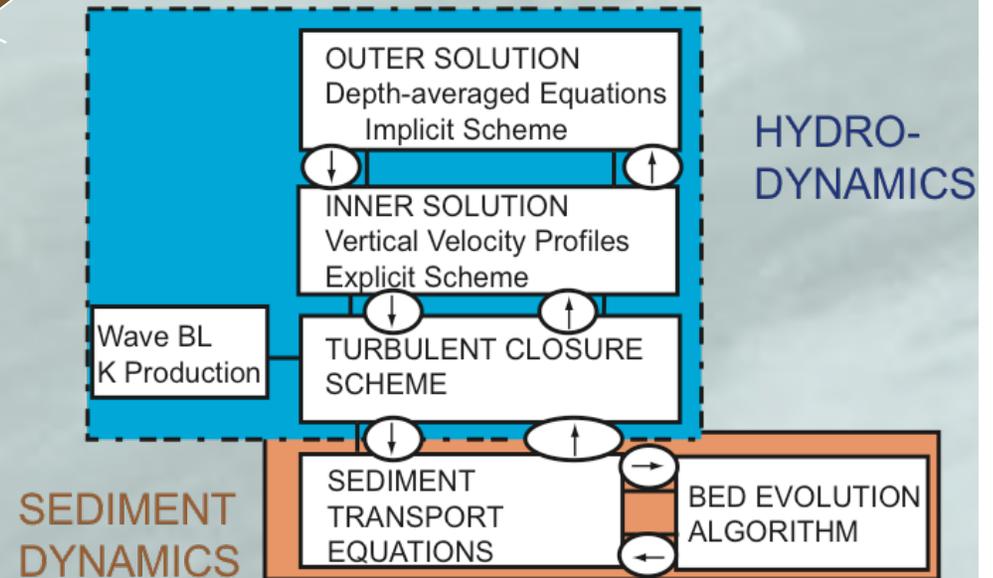


# SLICE Description

Neidoroda & Reed



SLICE (2d) MODEL



$$\frac{\partial c_i}{\partial t} + \frac{\partial u c_i}{\partial x} + \frac{\partial (w - w_{is}) c_i}{\partial z} = \frac{\partial}{\partial x} D_x \frac{\partial c_i}{\partial x} + \frac{\partial}{\partial z} D_z \frac{\partial c_i}{\partial z} + s_i - \lambda_i c_i$$

$$(w - w_{is}) c_i - D_z \frac{\partial c_i}{\partial z} = 0$$

Neidoroda & Reed

$$(w - w_{is}) c_i - D_z \frac{\partial c_i}{\partial z} = F_i$$

## SLICE Description

$$F_i = M(\tau_{ic}, \tau_b, \alpha_j)$$

$$\frac{\partial k}{\partial t} + \frac{\partial u k}{\partial x} + \frac{\partial w k}{\partial z} = \frac{\partial}{\partial x} \frac{K_x}{\sigma_x} \frac{\partial k}{\partial x} + \frac{\partial}{\partial z} \frac{K_z}{\sigma_z} \frac{\partial k}{\partial z} + P_k + G_k + P_{wc} - \frac{Cu''}{2} \frac{k^{3/2}}{\ell}$$

$$\ell = \frac{\alpha h_\ell k z}{\alpha h_\ell + k z}$$

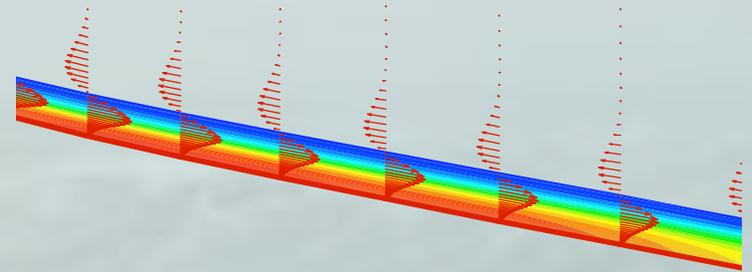
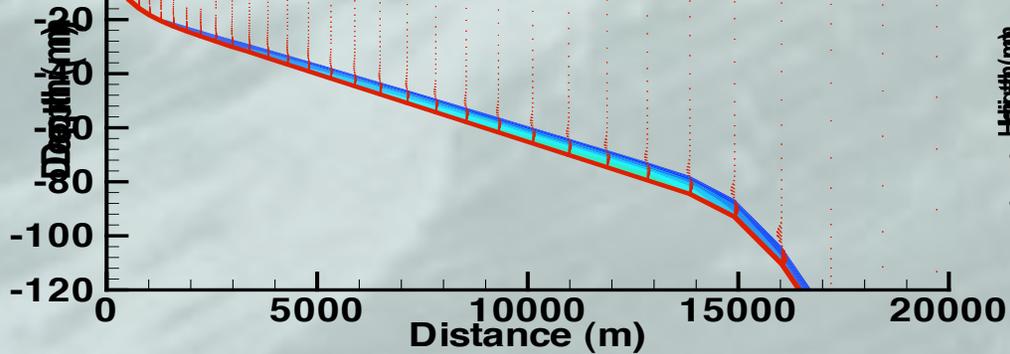
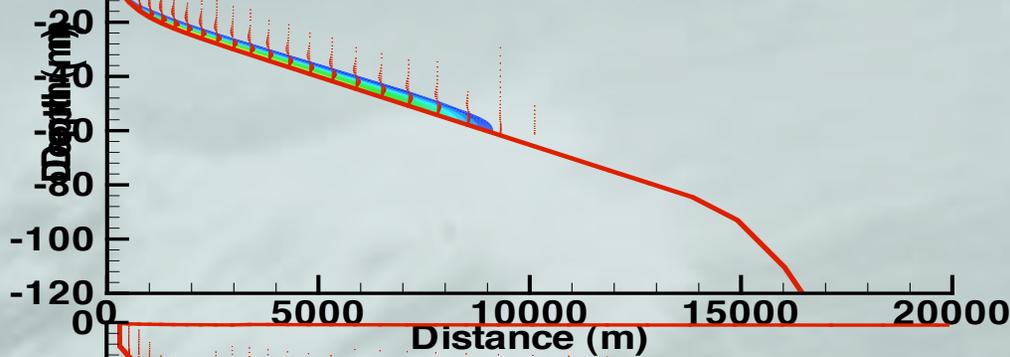
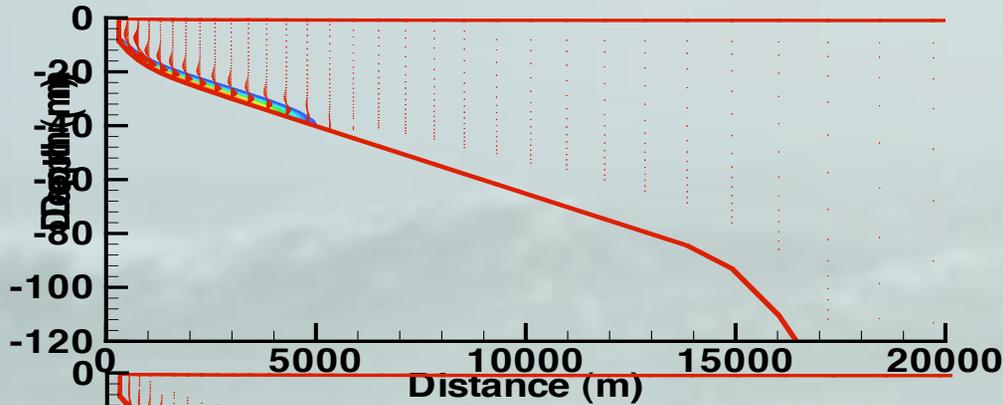
$$v_T = Cu' \sqrt{k} \ell$$

$$K_x = \text{constant}$$

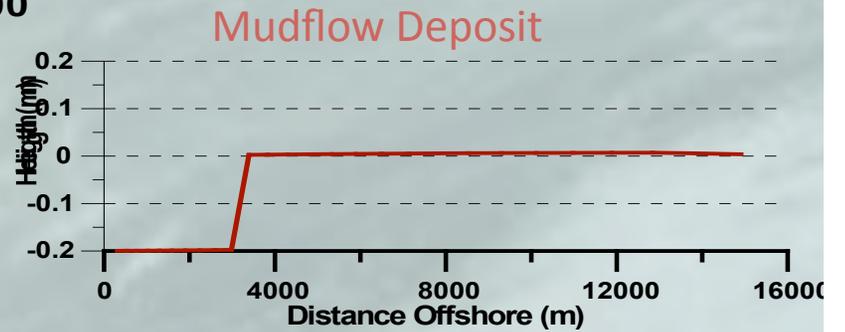
$$K_z = v + v_T$$



# SLICE Density Flows

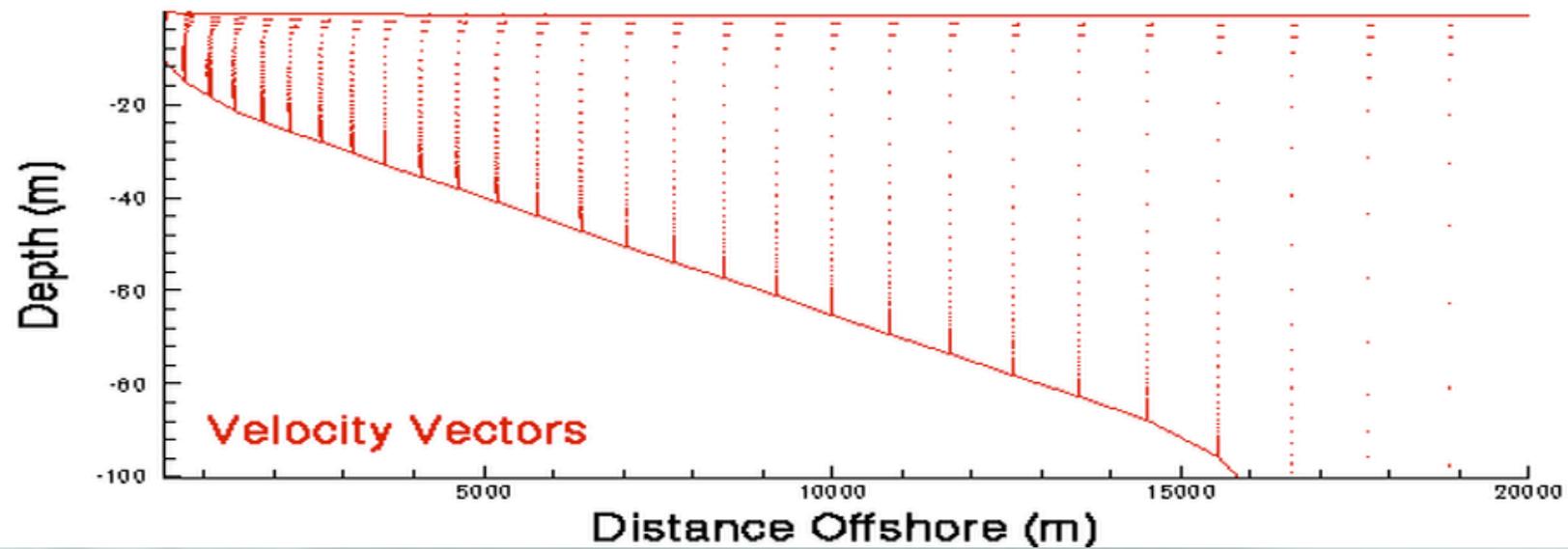
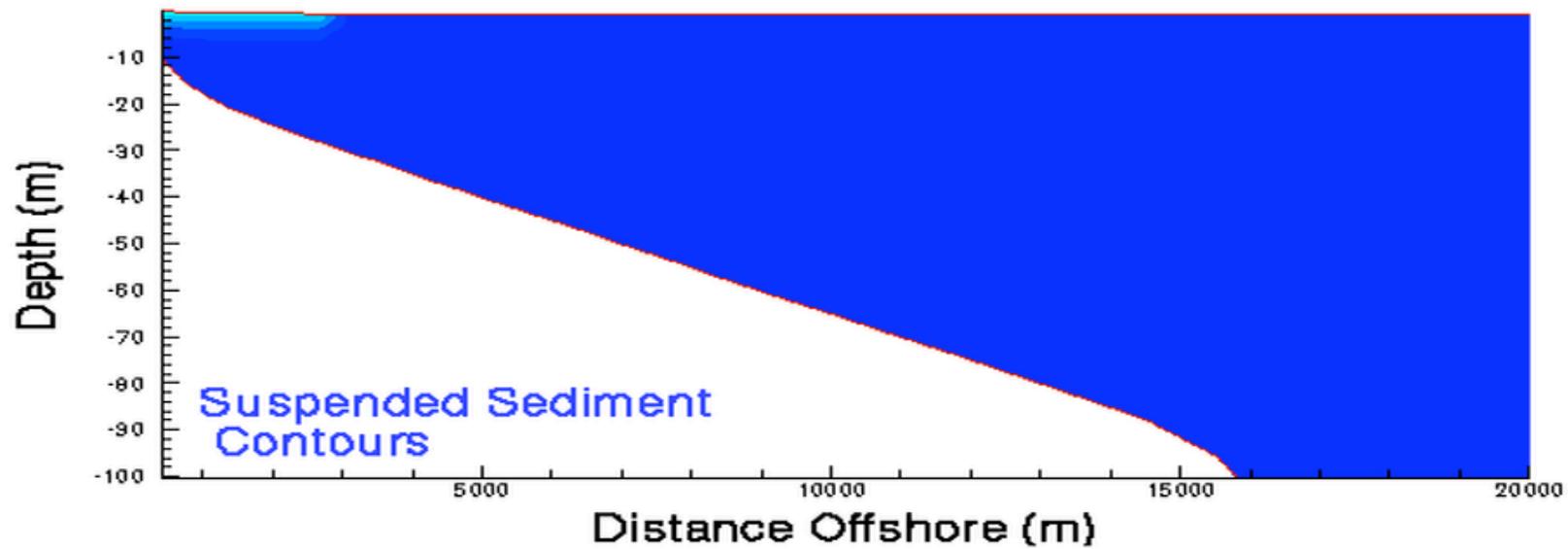


Mudflow Profile



Mudflow Deposit



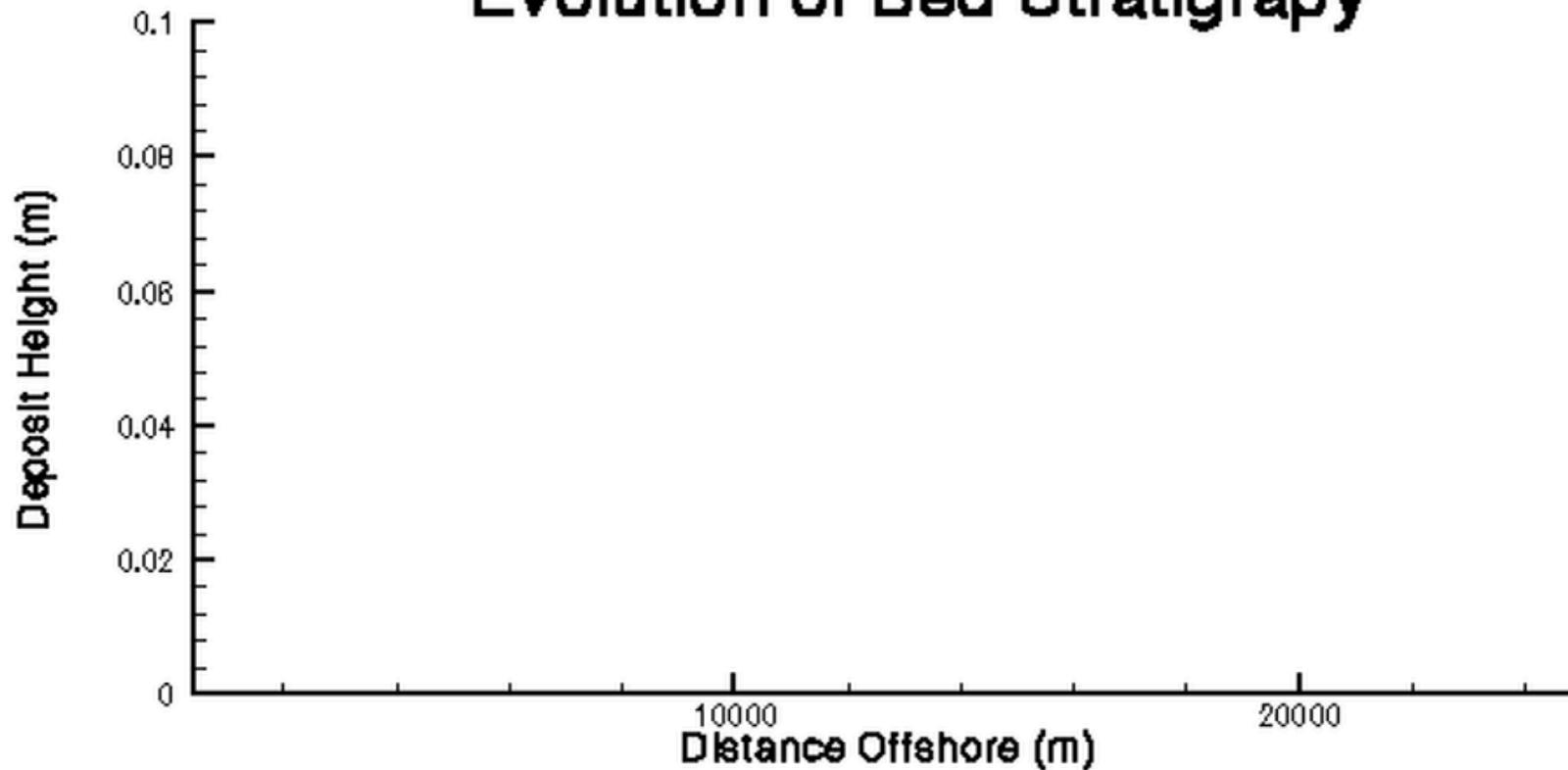


Neidoroda & Reed

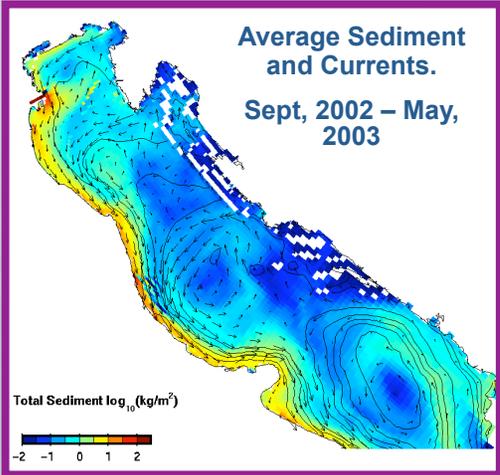
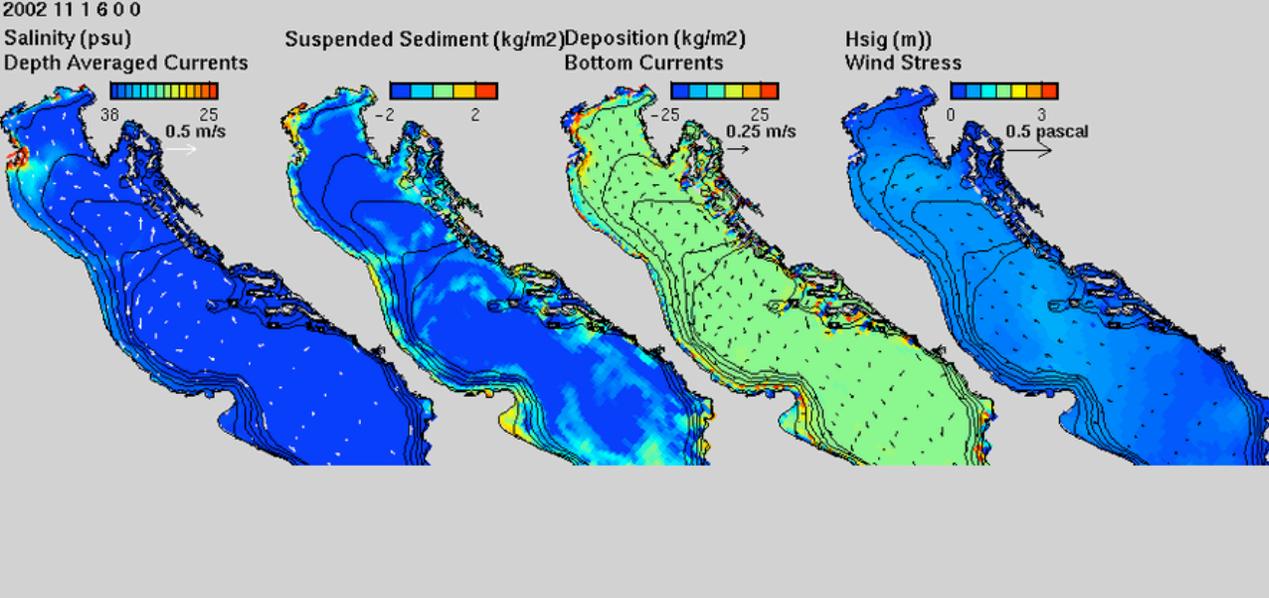
Earth-surface Dynamic Modeling & Model Coupling, 2009

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## Evolution of Bed Stratigraphy



# Nested Modeling



C.Harris, VIMS

Regional Hydrological Model (HydroTrend) (atm-landsurface model) to Regional Ocean Model (ROMS) for Sediment Supply, Buoyancy, Sediment Plumes

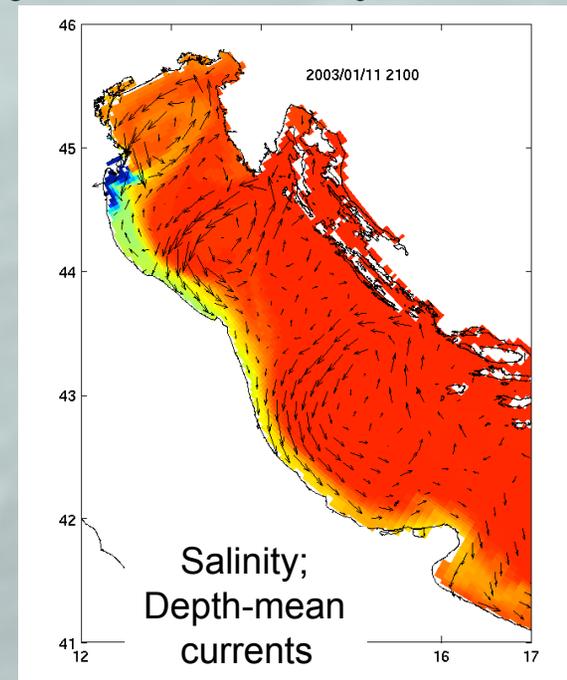
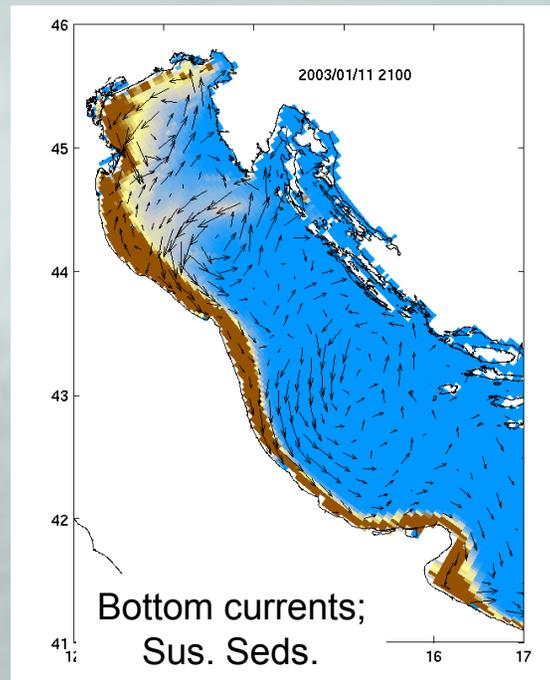
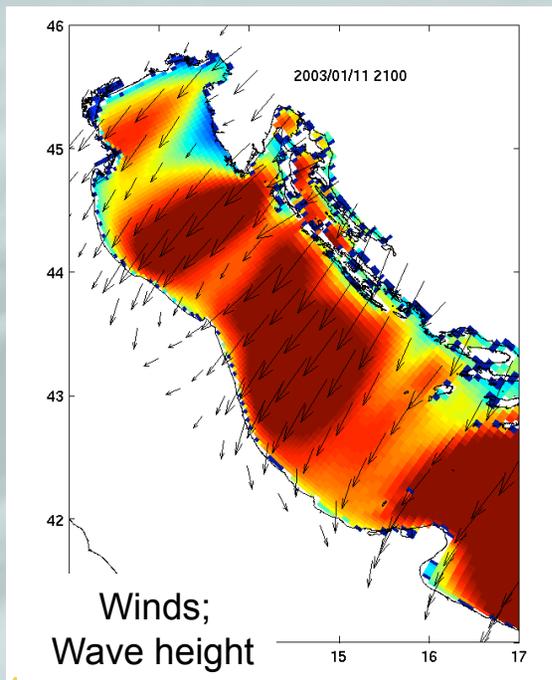
Global Ocean Model (NOGAPS) (coupled ocean-atm model) to Regional Ocean Model (ROMS) (coupled ocean-atm model) for Regional Circulation and Current Shear

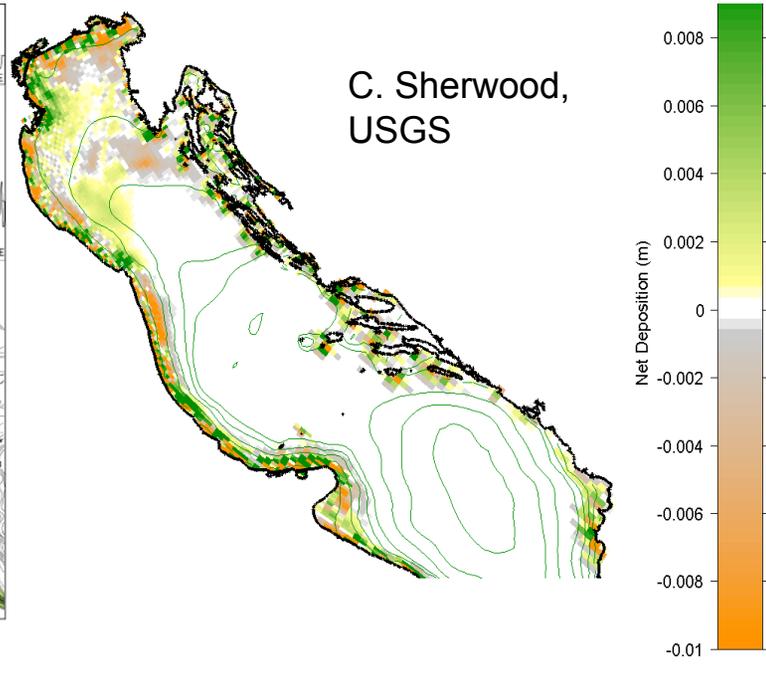
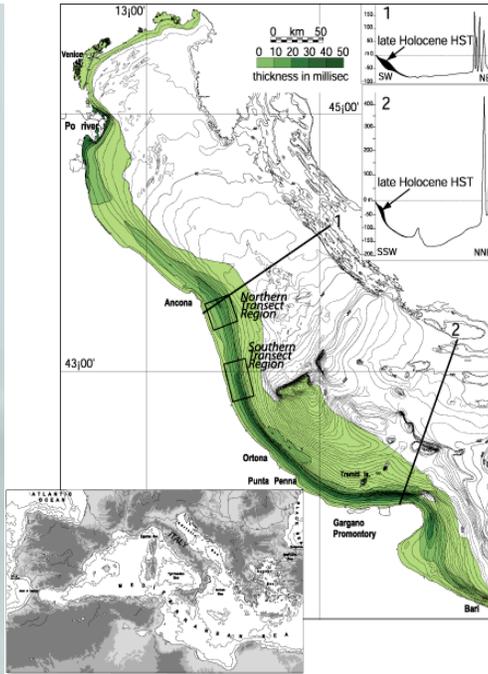
Global Met. Model (NOGAPS) (coupled ocean-atm model) to Regional Met. Model (COAMPS) (coupled ocean-atm model) to Wave Model (SWAN) for Sediment Resuspension (ROMS)



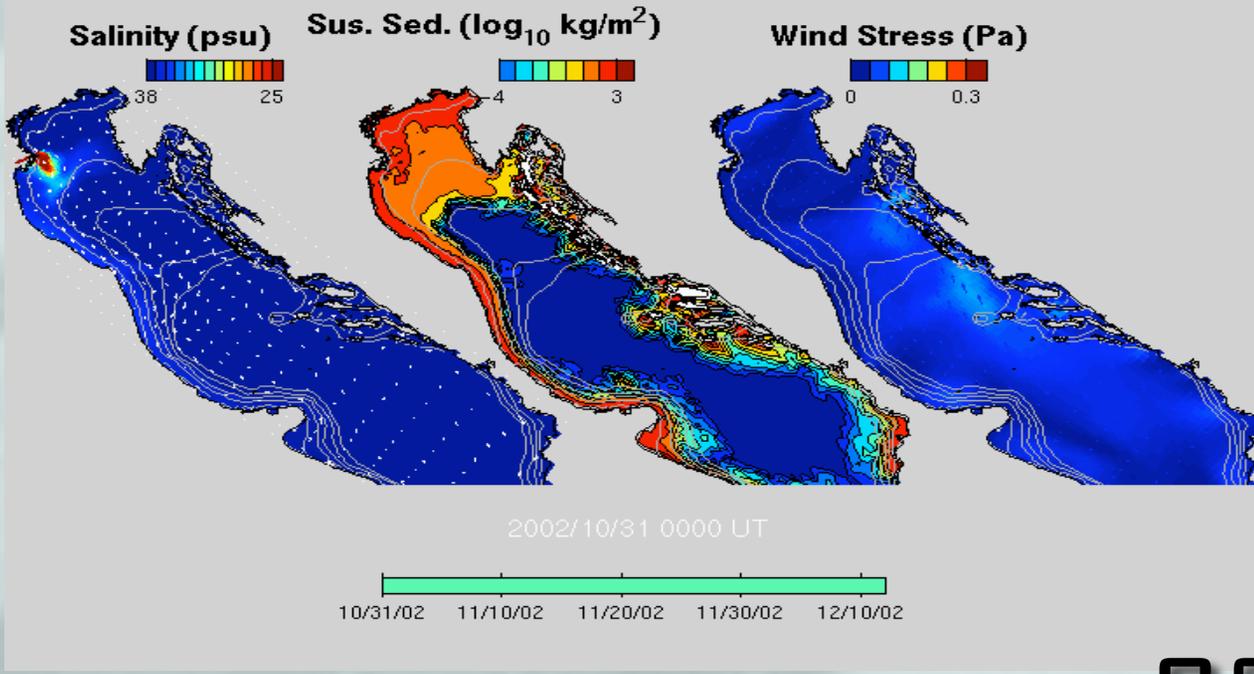
# Circulation and Sediment-Transport Modeling

- ROMS: Regional Ocean Modeling System — RANS for heat & momentum fluxes
- 3-8 km grid, 21 vertical “S” levels
- Initialized with ship data
- Zero-gradient b.c. near Otronto, seven tidal components
- LAMI forcing every 3 hours, SWAN waves, Po River discharge
- $k-\omega$  turbulence model, Styles & Glenn wave-current boundary layer
- Resuspension & transport of single grain size,  $w_s = 0.1$  mm/s,  $\tau_c = 0.08$  Pa

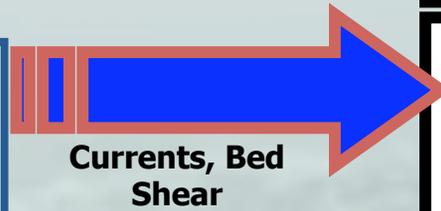
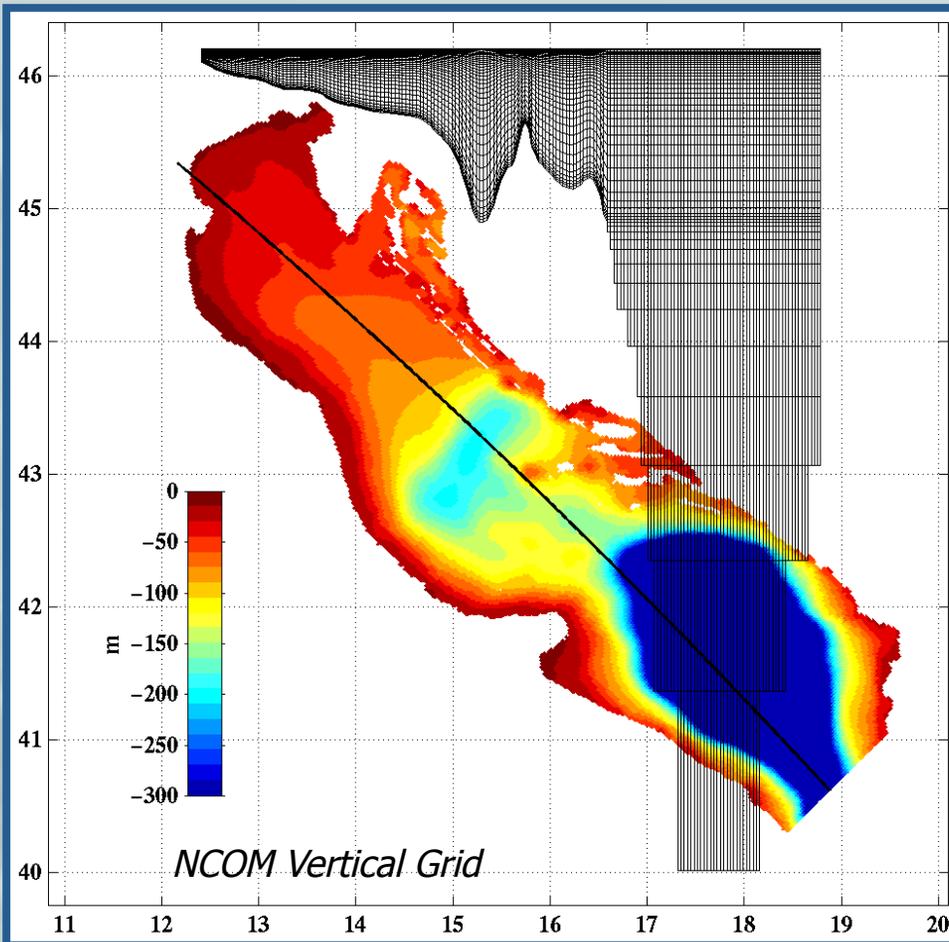




C. Sherwood,  
USGS



# VIMS-NCOM 3D Transport Model



## 2 km Sediment Model

Inputs: sediment sources, sizes, critical shear stress, settling velocity.

Calculates: flux, concentration, erosion / deposition.



Sea Floor Grid



# Conclusions:

## **Shelf diffusivity**

Advantages: uses daily *pdf* of regional ocean energy, simple and robust; compatible with landscape evolution models

Disadvantages: depends wave energy *pdf* -- how variable is diffusion in response to decadal and longer term variability?

## **Gravity-driven slope equilibrium**

Advantages: uses daily *pdf* of local total velocity, simple and robust; can be tested against field data

Disadvantages: Needs pdf for wave energy and sediment discharge from rivers, to calculate Richardson number

## **Event-based Approach**

Advantages: uses wave, current, and sediment information available for a site, preserving all correlations, can be tested against field data

Disadvantages: time scales short, data needs intensive for long-term simulations, inshore boundary condition difficult to specify

## **Coastal Ocean Model**

Advantages: Can get it right if all terms are included & appropriate resolution is used.

Disadvantage: Computationally intensive: data needs intensive

